

University of Idaho

College of Engineering

Design Review

Nick Daquila, Sean Blatner, Bryce Bilderback, Conner Krezman



Objective

• When traveling over bumpy surfaces with an unloaded forklift, the carriage and the forks tend to bounce violently. This creates a considerable amount of noise and increases wear on the system. The violent gyration can also cause an operator to spill what they are carrying. Our goal is to reduce the bounce of the carriage and the negative side effects ascertaining to carriage bounce.

Value Proposition

• Develop a carriage damping system to reduce/eliminate carriage bounce and vibration.

- Carriage bounce causes problems
 - Noise
 - Load instability
 - Increased wear
- We will use a brake mechanism to hold the carriage steady
 - Stop or reduce the motion of the carriage relative to the mast
- We will use a Fork clamp to reduce noise from rattling forks.
- reduce losses associated with unstable loads







Design requirements

- Effective on a variety of surfaces
 - Broken pallets, 2x4's, bumpy gravel lots, railroad tracks, etc.
- Within hydraulic pressures forklift is capable, ~2500 psi
- Work within \$4000 budget (\$2300 for materials, etc.)
- Scalable- Concept applicable to low and high-capacity trucks
- Manufacturable, fits on to current forklift design with minor changes
- Durable in outdoor conditions





Finalized Design-Fork Clamp







Finalized Design-Brake





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Manufacturing Plan

Part	Made Vs Bought	Part #	Material	Cost	Source	Qty.
Piston	Made	01-01	6061 AL	TBD	MetalSupermarkets	(
Cylinder	Made	01-02	6061 AL	TBD	MetalSupermarkets	2
Snap Ring	Bought	9560K450	PTFE	13.10 Per 50 pk	McMaster-Carr	(
O-Ring	Bought	94115K018	Neoprene	5.05 Per 100 pk	McMaster-Carr	(
Brake Pad	Made	01-03	6061 AL	TBD	MetalSupermarkets	
Retaining Plate	Made	01-04	Bronze	TBD	MetalSupermarkets	2
M4 Screws	Bought	92095A476	Steel	8.04 Per 100 pk	McMaster-Carr	5
M12 Bolts Class 10.9	Bought	97478A112	Steel	5.14	McMaster-Carr	4
M12 Pivot Bolt Grade 8	Bought	91257A561	Steel	6.04	McMaster-Carr	2
Thrust Bearing	Bought	3750K7	Iron Copper	2.75	McMaster-Carr	4
Grade 8 Locknut	Bought	90630A125	Steel	3.44 Per 10 pk	McMaster-Carr	4
Mil Spec Flat Washer	Bought	91922A307	Steel	9.32 Per 25 pk	McMaster-Carr	2
Retaining Ring	Bought	99142A350	Spring Steel	6.12 Per 50 pk	McMaster-Carr	2
Hex Nut	Bought	94846A520	Steel	6.22 Per 50 pk	McMaster-Carr	2
Tight Space Fitting 90 deg	Bought	6407T210	Steel	13.33	McMaster-Carr	2
Tight Space Fitting	Bought	6407T420	Steel	43.91	McMaster-Carr	2
Fork Piston	Made	02-01	Steel	TBD	MetalSupermarkets	2
Bottom Block	Made	02-02	Steel	TBD	MetalSupermarkets	



Spring Retaining Plate

- Used to hold piston return springs in place
- 1/16" air gap between pistons to prevent pistons from dragging and causing wear
- Held in place with 4 machine screws



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Cylinder

- Used 3 smaller pistons
- Rotates about corner
- Sleeved thrust bearings for support
- Made of Aluminum





Pistons

- 7/8" effective hydraulic diameter
- Springs used to return piston to un-extended position
- Buna-N O-ring seals coupled with backup rings
- Machined from 6061 Aluminum



Brake Foot

- Clamps outside of mast to hold carriage in place
- Holds replaceable brake pad
- Machined from 6061 Aluminum



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Brake Positions



Clamped Position



Unclamped Position



Pivot Design

- Pivoting the brake when not in use provides ¼" clearance along the length of the J-Channel mast so the brake pad does not wear in travel
- Allows for a deviation in thickness of J-channel
- Uses oil-impregnated bushings to reduce friction and wear





O-Rings

- 018 O-ring used for Carriage clamp
- Breakout Friction is approximately 3 times running friction
- Running Friction is FH + Fc = fh x Ap + fc x Lp
- Based on surface finish and final rubber, the force to overcome can range from 36 lbs to 72 lbs

- F =Total seal friction in pounds.Fc =Total friction due to seal compression.FH =Total friction due to hydraulic pressure on the seal.
- fc = Friction due to O-ring compression obtained from Figure A6-5.
- fh = Friction due to fluid pressure obtained from Figure A6-6.
- Lp = Length of seal rubbing surface in inches for piston groove applications.
- Lr = Length of seal rubbing surface in inches for rod groove applications.





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Springs

- Assuming the pressure from the fluid is negligible there are several springs that could return the pistons
- Only between .12 to .25 inches of travel is needed

Product ~	CAD / Specs	<u>Material</u> ~	<u>Wire Dia (in)</u> √	<u>O. D. (in)</u> ~	<u>I. D. (in)</u> ~	<u>Free Length (in)</u> ~	<u>Total Coils</u> √	<u>Rate (Ib/in)</u> ~	Ends ~	Suggested Max Load (Ib) ~	Suggested Max Deflection (in) ~	<u>Solid Length (in)</u> √	<u>Standard Finish</u> ~	Buy
□ NN-24	\otimes	Spring Steel - SPR	0.160	0.953	0.633	0.690	3.25	1,511.00	Closed/Ground - CG	124.000	0.080	0.52	Gold Irridite - Gl]_
MM-98	\otimes	Spring Steel - SPR	0.150	1.031	0.731	0.690	3.50	710.00	Closed/Ground - CG	96.000	0.130	0.53	Zinc - Z	F
☐ KK-54	\otimes	Spring Steel - SPR	0.140	0.968	0.688	0.780	4.00	486.00	Closed/Ground - CG	85.000	0.170	0.56	Gold Irridite - Gl	Ì
10942	\otimes	Spring Steel - SPR	0.135	0.875	0.605	0.690	3.00	1,178.00	Closed/Ground - CG	84.000	0.070	0.41	Zinc - Z	F
4235	\otimes	Spring Steel - SPR	0.135	0.938	0.668	0.750	3.50	615.00	Closed/Ground - CG	79.000	0.130	0.47	Zinc - Z]
2817	\otimes	Music Wire - MW	0.110	0.921	0.701	0.500	3.00	395.00	Closed/Ground - CG	63.000	0.160	0.33	Zinc - Z	F
□S-3040	\$	Stainless Steel - SST	0.130	0.938	0.678	0.750	3.50	451.00	Closed/Ground - CG	63.000	0.140	0.46	None - N	F
3702	\$	Spring Steel - SPR	0.120	0.875	0.635	0.660	4.00	346.00	Closed/Ground - CG	61.000	0.180	0.48	Zinc - Z	F
A11-51	\$	Spring Steel - SPR	0.121	0.906	0.664	0.750	4.00	340.00	Closed/Ground - CG	61.000	0.180	0.47	Zinc - Z	F
AA-59	\$	Spring Steel - SPR	0.120	0.859	0.619	0.630	4.00	369.00	Closed/Ground - CG	54.000	0.150	0.48	Gold Irridite - Gl	F
AA-64	\$	Spring Steel - SPR	0.130	0.890	0.630	0.630	4.00	468.00	Closed/Ground - CG	49.000	0.110	0.52	Zinc - Z	F
2766	\$	Spring Steel - SPR	0.110	0.906	0.686	0.500	3.00	417.00	Closed/Ground - CG	46.000	0.110	0.33	Zinc - Z	F
1581	\otimes	Spring Steel - SPR	0.105	0.859	0.649	0.630	3.50	272.00	Closed - C	41.000	0.150	0.47	Zinc - Z	



Brake Calculations

Diameter	Area	Pressure	Friction Coefficient	Friction Coefficient
0.875 in	0.60 in^2	2500 psi	0.16	0.61
			Steel on Steel greased	Steel on aluminum
Force per cylinder			Hold Force per brake pad	
1503 lb			2751 lb	
			Hold Force for 3 pistons	
			721 lb	
			Total Hold Force	
			6945 lb	



Bolt Calculations

- 12mm x 90mm bolts provide a Load Factor over 2
- Goodman Failure Criteria yields an infinite lifetime with a 1.27 Factor of Safety

Inputs			Design				•	4	451	0 lbs	Total			
E =	2.00E+07 psi	Elastic modulus of the clamping mat	erial n =	2	load factor									
E _b =	3.00E+07 psi	Elastic modulus of the bolt material	N =	2	Number of bolts									
S _p =	140687 psi	Proof strength of the bolt material					1.5 in.							
d =	0.4700 in	bolt size	F ; =	13791 lbs	Initial load (per bolt)									
A _t =	0.1307 in ²	Tensile area of the bolt							shear					
L =	3.54 in	Length of the bolt	T=	1296 in-lk	Tightening Torque				112	7 lbs				
1=	3.00 <u>i</u> n	grip length		108 ft-lb	FI	b = Fi + Pb	_		i				= Fi + Pb	
	0.540 in	extension of bolt beyond the grip	F =	-9652 lbs	(needs to be negative)	14750	lbs 🛉						14750 l	bs
	Need to make su	re this is enough for a nut (or tapped a	hreads)											
Calculated			F _b =	14750 lbs			1.19 in.							
A _d =	0.1735	Tensile area of the shank					↓						Normal	
I _{th} =	1.19 in	Length of bolt threads (if bolt is < 6") P =	10195 lbs	Total Separation force			0					Stress =	112853 psi
1 _d =	2.35 in	Length of shank												
			P _N =	5097 lbs	Separation force per bolt		Sum M_O							
I _{thg} =	0.65 in	Length of threads in the grip					P = 10195 lk	os Total						
	Need to make su	re this is above zero.	This is the P	roof load for eac	n bolt:					Need to	use tao = VQ	/Ib to get	the shear st	ress,
			P _{max} =	12217 lbs	Load each bolt can carry						but this is	ikely very	small.	
Results				Compare this t	o P _N (should be higher)					•				
k _b =	1.62E+06 in-lb							•	-	-		112853		
k _ =	6.99E+06 in-lb		This is the f	orce required for	unclamping for each bolt:				•					
C =	0.188		P ₀ =	8493 Lbs										
1-C =	0.812			Compare this t	o P _N (should be higher)						von Mises	112853	psi	
				•		++							i de la companya de l	



Validation Plan

- FEA
- Strain gauge measurements
- Full-scale, functional prototype
- Installed on a forklift carriage





Carraige FEA

Stress Test R	lesults
Config	Stress (Mpa)
Base	56.0
	74.3
	48.8
	60.0
Вох	32.6
	57.5
	49.7
	64.6
Hole	50.4
	58.8
	63.2
	70.2







Cylinder FEA

- Tested using max holding force
- Plan to account for bolt pre-load
- Need to rework control volume





Data Collection

- What?
 - Inertial load determination
- Why?
 - Design Validation
- How?
 - Accelerometers
 - Strain Gauge





Accelerometer Data Collection

Limitations:

- I2C protocol noise
- Collisions
- Advantages:
- Fast, easy data
- All components on-hand







Data Collection

- Wheatstone Bridge and Rosette Gauges
- Strain Gauges will be attached to the chain anchors
- Voltage data collected with LabView and a National Instruments DAQ
- Collected data can be analyzed with MATLAB
- Will need to take spring rate of the leaf chain into consideration when performing analysis



Experiment Design

- Items to run over:
 - 2x4
 - Pallet Board
 - Extension cord
 - Air hose
 - Gravel lot
 - Large pothole

- Loads to test:
 - Unloaded
 - The forklift we have access to has a rotator attachment
 - 1000 pound load
 - 2000 pound load
 - 3000 pound load



Data Collection: Current progress



Materials have arrived



Developing LabView Data Acquisition Code



Forward Looking: Data Collection and Analysis



Full Scale Prototype

- Receiving carriage and forks from HYG
- Installing prototype
- Return to HYG to be installed on Forklift
- Test at HYG location with or without us depending on Covid-19 development



Potential Risks

- Hydraulic power requirements may take away the ability to add other auxiliary functions
- Wear on the mast J-Channel can compromise the integrity over time
- Increased Maintenace costs
- Adding rigidity to the system may cause unforeseen consequences
 - Less give in the system causing increased wear on components

Project Budget

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Capstone Project Budg	et Templat	te - Fall/S	pring									
Project:												
Last Updated	2/24/2021											
				Yea	ir 👘					Item		
Expense Items	Sept	Oct	Nov	Dec	Jan	Feb	Mar	Apr		Total		
Equipment/Tools:												
Strain Measurement		\$ 43			\$ 388				\$	431		
Equipment/Tools												
Travel:												
									\$	-		
									\$	-		
Supplies / Parts / Services:												
facilities machining									Ś	-		
Supplies / Parts / Services							\$ 213		\$	213		
Fittings							\$ 40		Ś	40		
Hoses							\$ 200		\$	200		
Aluminum Stock							\$ 200		\$	200		
Steel Stock							\$ 50		\$	50		
Hardware							\$ 75		\$	75		
Nuts and Bolts							\$ 25		\$	25		
Hydraulic Pump							\$ 200		\$	200		
Seals							\$ 38		\$	38		Expenses
Springs							\$ 100				\$ 1,472	Subtotal
Shop Usage (est. Hrs):										Hours		
Shop time							30			30		
										0		
										0		
										0		
										0		
										0		
						Grad	duate Stude	ent Support	Ś	1.021	including	fringe
						2.44	Shor	Overhead	Ś	500		
							University	y Overhead	\$	150	5% of all e	expenses
								Totals	\$	3,142	\$ 4,000	\$ 858
											Budget	Excess



Project Schedule

		Project:	Hyste	r Yale	e Carri	age B	Bounce	Con	trol Svs	stem																										
	Las	t Updated:	ted: 2/24/20										_																							
		Year		-							2020															20	21									
		Month		Se	pt			00	:t			N	lov			Dec		Jan Feb					Mar Apr								May	,				
Task Description	Duration	Assigned	9/4	9/13	9/20	9/27	10/4	10/11	10/18 1	0/25	11/1	11/8 11	/15 1	1/22 11/2	29 12/6	12/13 12/2	0 12/27	1/3 1/10	1/17 1/	/24 1/3	31 2/	7 2/1	4 2/21	2/28	3/7	3/14	3/21	3/28	4/4	4/11 4/	18 4/2	5 5/	2 5/9	5/16	5/23	3 5/30
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Questions?